

Mct/ROB/200 Robotics, Spring Term 12-13

Lecture 4 – Friday March 15, 2012

# **Forward Kinematics**

# **Objectives**

When you have finished this lecture you should be able to:

• Learn how to derive the forward kinematic equations of the robot using Denavit-Hartenberg (D-H) representation technique.

## Outline

- Forward Kinematics
- Denavit-Hartenberg Algorithm
- Summary

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## **Forward Kinematics**



**Given:** The angle of each joint **Required:** The position of end-effector or any point (i.e. its coordinates)  $(p_x,p_y,p_z,\phi,\theta,\psi)$ 

Forward Kinematics



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#### **Required:**

$$p_{x}=f_{x} (\theta_{1}, \theta_{2}, \theta_{3}, \theta_{4}, \theta_{5}, \theta_{6})$$

$$p_{y}=f_{y} (\theta_{1}, \theta_{2}, \theta_{3}, \theta_{4}, \theta_{5}, \theta_{6})$$

$$p_{z}=f_{z} (\theta_{1}, \theta_{2}, \theta_{3}, \theta_{4}, \theta_{5}, \theta_{6})$$

$$\phi=f_{\phi} (\theta_{1}, \theta_{2}, \theta_{3}, \theta_{4}, \theta_{5}, \theta_{6})$$

$$\theta=f_{\theta} (\theta_{1}, \theta_{2}, \theta_{3}, \theta_{4}, \theta_{5}, \theta_{6})$$

$$\psi=f_{\psi} (\theta_{1}, \theta_{2}, \theta_{3}, \theta_{4}, \theta_{5}, \theta_{6})$$

Cartesian Space

# **Forward Kinematics**

• A Plan Arm with 2-DOF Given:  $\theta_1, \theta_2$ 

Required: x, y

Solution:



#### **Trigonometric Solution**

 $\begin{aligned} x = l_1 \cdot \cos\theta_1 + l_2 \cos(\theta_1 + \theta_2) \\ y = l_1 \cdot \sin\theta_1 + l_2 \sin(\theta_1 + \theta_2) \end{aligned}$ 

See Trigonometric Solution.xls

**Algebraic Solution** 

$${}^{0}T_{2} = {}^{0}T_{1} {}^{1}T_{2}$$

# **Forward Kinematics**

- A Plan Robot with 3-DOF
- **Given:**  $\theta_1, \theta_2, \theta_3, l_1, l_2, l_3$
- Required: x, y



### Solution:



## Outline

• Forward Kinematics

### Denavit-Hartenberg Algorithm

• Summary





### Analyzing the robot morphology



Axis of motion is in the direction of rotation as followed by the righthand rule for rotations.





**Prismatic Joint** 1 DOF (linear) (Variable - d)

Axis of motion is along the direction of the linear movement.

#### Analyzing the robot morphology



**D-H 1:** Give a number for each joint from 1 to N starting with the base and ending with the tool yaw, pitch, and roll, in that order

#### Establishing Coordinate Systems



#### Establishing Coordinate Systems



#### Establishing Coordinate Systems



 $Z_{U}$ 

#### Establishing Coordinate Systems



 $Z_{U}$ 

#### Establishing Coordinate Systems



 $Z_{U}$ 

Calculate D-H Parameters



Calculate D-H Parameters



Calculate D-H Parameters

di

make X<sub>i-1</sub> and X<sub>i</sub> aligned



Η

 $\theta_4$ 

 $1_{4}$ 

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Calculate D-H Parameters







Calculate D-H Parameters



#### Calculate D-H Parameters



Η

 $\theta_4$ 

 $l_{\Delta}$ 

Rx

 $\alpha_i$ 

0

-90°

0

0

0

#### D-H Transformation Matrix

D-H Transformation Matrix for adjacent coordinates frames, i and i-1

$${}^{i-1}A_i = \begin{bmatrix} C\theta_i & -C\alpha_i S\theta_i & S\alpha_i S\theta_i & a_i C\theta_i \\ S\theta_i & C\alpha_i C\theta_i & -S\alpha_i C\theta_i & a_i S\theta_i \\ 0 & S\alpha_i & C\alpha_i & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix} \xrightarrow{z_{n-1}} {}^{z_{n-1}} \xrightarrow{\theta_{n+1}} \xrightarrow{z_{n+1}} {}^{z_{n+1}} \xrightarrow{y_{n+1}} \xrightarrow{y_{n+1}} {}^{z_{n+1}} \xrightarrow{z_{n+1}} \xrightarrow{y_{n+1}} \xrightarrow{y_{n+1}} \xrightarrow{z_{n+1}} \xrightarrow{z_{n+1}} \xrightarrow{y_{n+1}} \xrightarrow{z_{n+1}} \xrightarrow{z_$$

Total Transformation between the base of the robot and the hand is:

$${}^{R}T_{H} = {}^{O}A_{n} = {}^{O}A_{1} \cdot {}^{1}A_{2} \cdot {}^{2}A_{3} \cdot \dots \cdot {}^{(n-1)}A_{n}$$

#### • D-H Transformation Matrix

**Partial Matrices** 

$${}^{i-1}A_{i} = \begin{bmatrix} C\theta_{i} & -C\alpha_{i}S\theta_{i} & S\alpha_{i}S\theta_{i} & a_{i}C\theta_{i} \\ S\theta_{i} & C\alpha_{i}C\theta_{i} & -S\alpha_{i}C\theta_{i} & a_{i}S\theta_{i} \\ 0 & S\alpha_{i} & C\alpha_{i} & d_{i} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

RzTzTxRxi $\theta_i$  $d_i$  $a_i$  $\alpha_i$ 1 $\theta_1$  $1_1$ 00

 $d_2$ 

 $d_3$ 

 $l_{4}$ 

0

0

0

90°

0

 $\theta_{4}$ 

2

3

Η

$${}^{0}A_{1} = \begin{bmatrix} C\theta_{1} & -S\theta_{1} & 0 & 0 \\ S\theta_{1} & C\theta_{1} & 0 & 0 \\ 0 & 0 & 1 & l_{1} \\ 0 & 0 & 0 & 1 \end{bmatrix} {}^{1}A_{2} = \begin{bmatrix} 0 & 0 & 1 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & d_{2} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

-90°

0

0

#### • D-H Transformation Matrix

**Partial Matrices** 

$${}^{i-1}A_{i} = \begin{bmatrix} C\theta_{i} & -C\alpha_{i}S\theta_{i} & S\alpha_{i}S\theta_{i} & a_{i}C\theta_{i} \\ S\theta_{i} & C\alpha_{i}C\theta_{i} & -S\alpha_{i}C\theta_{i} & a_{i}S\theta_{i} \\ 0 & S\alpha_{i} & C\alpha_{i} & d_{i} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

	Rz	Tz	Tx	Rx
i	$\theta_{i}$	d <sub>i</sub>	a <sub>i</sub>	$\alpha_{i}$
1	$\theta_1$	$l_1$	0	0
2	90°	$d_2$	0	-90°
3	0	d <sub>3</sub>	0	0
Η	$\theta_4$	$l_4$	0	0

$${}^{2}A_{3} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d_{3} \\ 0 & 0 & 0 & 1 \end{bmatrix} {}^{3}A_{H} = \begin{bmatrix} C\theta_{4} & -S\theta_{4} & 0 & 0 \\ S\theta_{4} & C\theta_{4} & 0 & 0 \\ 0 & 0 & 1 & l_{4} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

#### • D-H Transformation Matrix

**Total Transformation Matrix** 

 ${}^{R}T_{H} = {}^{0}A_{4} = {}^{0}A_{1} \cdot {}^{1}A_{2} \cdot {}^{2}A_{3} \cdot {}^{3}A_{4}$ 

$${}^{R}T_{H} = {}^{0}A_{H} = \begin{bmatrix} -S_{1}C_{4} & S_{1}S_{4} & C_{1} & C_{1}(d_{3}+l_{4}) \\ C_{1}C_{4} & -C_{1}S_{4} & S_{1} & S_{1}(d_{3}+l_{4}) \\ S_{4} & C_{4} & 0 & d_{2}+l_{1} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

#### • ABB IRB 1400

![](_page_28_Figure_2.jpeg)

ABB IRB 1400

#### • ABB IRB 1400

For this ABB IRB 1400 robot:

- Assign the coordinate frames based on the D-H representation;
- Fill out the parameters table;
- Write all the A matrices;
- Write the total transformation matrix in terms of the A matrices.

#### ABB IRB 1400: Frame Assignment

#### **Assigning Frame-0:**

The given first frame will be considered as the base frame.

 $Z_o$  is the axis of actuation for joint 1. Its direction will be as shown in the figure.

We may choose the origin  $O_o$  of the base frame to be any point on  $Z_o$ .

We then choose  $X_o$  (and  $Y_o$  if you want) in any convenient manner as long as the resulting frame is right-handed. In this problem, the direction of  $X_o$  is already given. This sets up frame 0.

![](_page_30_Figure_7.jpeg)

![](_page_30_Figure_8.jpeg)

### ABB IRB 1400: Frame Assignment

### **Assigning Frame-1:**

 $Z_1$  is the axis of actuation for joint 2. Its direction will be as shown in the figure.

 $Z_1$  and  $Z_0$  are parallel. In this case, there are infinitely many common normals between them. In this case we are free to choose the **origin O**<sub>1</sub> **anywhere along Z**<sub>1</sub>. One often chooses O<sub>1</sub> to simplify the resulting equations.

![](_page_31_Figure_5.jpeg)

### ABB IRB 1400: Frame Assignment

### **Assigning Frame-1:**

The axis  $X_1$  is then chosen either to be **directed from O**<sub>1</sub> toward  $Z_0$ , along the common normal, or as the **opposite** of this vector.

A common method for choosing  $O_1$  is to choose the normal that passes through  $O_0$  as the  $X_1$  axis;  $O_1$  is then the point at which this normal intersects  $Z_1$ . Following these rules,  $O_1$  and  $X_1$  are chosen as shown in the figure. This sets up frame 1.

![](_page_32_Figure_5.jpeg)

#### ABB IRB 1400: Frame Assignment

### **Assigning Frame-2:**

 $Z_2$  is the axis of actuation for joint 3. Its direction will be as shown in the figure.

 $Z_2$  and  $Z_1$  are parallel. In this case, there are infinitely many common normals between them. In this case we are free to choose the origin  $O_2$  anywhere along  $Z_2$ . One often chooses  $O_2$  to simplify the resulting equations.

![](_page_33_Figure_5.jpeg)

### ABB IRB 1400: Frame Assignment

### **Assigning Frame-2:**

The axis  $X_2$  is then chosen either to be directed from  $O_2$  toward  $Z_1$ , along the common normal, or as the opposite of this vector.

A common method for choosing  $O_2$  is to choose the normal that passes through  $O_1$  as the  $X_2$  axis;  $O_2$  is then the point at which this normal intersects  $Z_2$ . Following these rules,  $O_2$  and  $X_2$  are chosen as shown in the figure. This sets up frame 2.

![](_page_34_Figure_5.jpeg)

### ABB IRB 1400: Frame Assignment

### **Assigning Frame-3:**

 $Z_3$  is the axis of actuation for joint 4. Its direction will be as shown in the figure.

 $Z_3$  and  $Z_2$  are parallel. In this case, there are infinitely many common normals between them. In this case we are free to choose the **origin**  $O_3$  **anywhere along**  $Z_3$ . One often chooses  $O_3$  to simplify the resulting equations.

![](_page_35_Figure_5.jpeg)

### ABB IRB 1400: Frame Assignment

### **Assigning Frame-3:**

The axis  $X_3$  is then chosen either to be directed from  $O_3$  toward  $Z_2$ , along the common normal, or as the opposite of this vector.

A common method for choosing  $O_3$  is to choose the normal that passes through  $O_2$  as the  $X_3$  axis;  $O_3$  is then the point at which this normal intersects  $Z_3$ . Following these rules,  $O_3$  and  $X_3$  are chosen as shown in the figure. This sets up frame 3.

![](_page_36_Figure_5.jpeg)

### ABB IRB 1400: Frame Assignment

### **Assigning Frame-4:**

 $Z_4$  is the axis of actuation for joint 5. Its direction will be as shown in the figure.

**Z**<sub>4</sub> and **Z**<sub>3</sub> intersect. In this case,  $X_4$  is chosen normal to the plane formed by  $Z_4$  and  $Z_3$ . The positive direction of  $X_4$  is arbitrary.

The most natural choice for the origin  $O_4$ in this case is at the point of intersection <sup>1</sup> of  $Z_4$  and  $Z_3$ . However, any convenient point along the axis  $Z_4$  suffices. This sets up frame 4.

![](_page_37_Figure_6.jpeg)

l<sub>1</sub>

### ABB IRB 1400: Frame Assignment

### **Assigning Frame-5:**

 $Z_5$  is the axis of actuation for joint 6. Its direction will be as shown in the figure.

 $Z_5$  and  $Z_4$  intersect. In this case,  $X_5$  is chosen normal to the plane formed by  $Z_5$ and  $Z_4$ . The positive direction of  $X_5$  is arbitrary.

![](_page_38_Figure_5.jpeg)

h

#### ABB IRB 1400: Frame Assignment

### **Assigning Frame-5:**

The most natural choice for the origin  $O_5$  in this case is at the point of intersection of  $Z_5$  and  $Z_4$ . However, any convenient point along the axis  $Z_5$  suffices. This sets up frame 5.

![](_page_39_Figure_4.jpeg)

#### ABB IRB 1400: Frame Assignment

![](_page_40_Figure_2.jpeg)

#### ABB IRB 1400: Frame Assignment

![](_page_41_Figure_2.jpeg)

**D-H 6:** Locate point b<sub>i</sub> at the intersection of X<sub>i</sub> and  $Z_{i-1}$  axes. If they do not intersect, use the intersection of X<sub>i</sub> with a common normal between  $X_i$  and  $Z_{i-1}$ .

 $\mathbb{Z}_5$ 

 $\mathbf{b}_1$ 

![](_page_42_Figure_2.jpeg)

#### • ABB IRB 1400: D-H Parameter Table

![](_page_43_Figure_2.jpeg)

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 $\alpha_{i}$ 

![](_page_44_Figure_2.jpeg)

![](_page_45_Figure_2.jpeg)

![](_page_46_Figure_2.jpeg)

![](_page_47_Figure_2.jpeg)

#### ABB IRB 1400: Partial/Adjacent Matrices

$${}^{i-1}A_{i} = \begin{bmatrix} C\theta_{i} & -C\alpha_{i}S\theta_{i} & S\alpha_{i}S\theta_{i} & a_{i}C\theta_{i} \\ S\theta_{i} & C\alpha_{i}C\theta_{i} & -S\alpha_{i}C\theta_{i} & a_{i}S\theta_{i} \\ 0 & S\alpha_{i} & C\alpha_{i} & d_{i} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^{0}A_{1} = \begin{bmatrix} C_{1} & 0 & S_{1} & l_{2}C_{1} \\ S_{1} & 0 & -C_{1} & l_{2}S_{1} \\ 0 & 1 & 0 & l_{1} \\ 0 & 0 & 0 & 1 \end{bmatrix} {}^{1}A_{2} = \begin{bmatrix} C_{2} & -S_{2} & 0 & l_{3}C_{2} \\ S_{2} & C_{2} & 0 & l_{3}S_{2} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

ABB IRB 1400: Partial/Adjacent Matrices

$${}^{4}\mathbf{A}_{5} = \begin{bmatrix} \mathbf{C}_{5} & \mathbf{0} & \mathbf{S}_{5} & \mathbf{0} \\ \mathbf{S}_{5} & \mathbf{0} & -\mathbf{C}_{5} & \mathbf{0} \\ \mathbf{0} & \mathbf{1} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{1} \end{bmatrix} {}^{2}\mathbf{A}_{3} = \begin{bmatrix} \mathbf{C}_{3} & \mathbf{0} & \mathbf{S}_{3} & \mathbf{1}_{4}\mathbf{C}_{3} \\ \mathbf{S}_{3} & \mathbf{0} & -\mathbf{C}_{3} & \mathbf{1}_{4}\mathbf{S}_{3} \\ \mathbf{0} & \mathbf{1} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{1} \end{bmatrix}$$

$${}^{3}\mathbf{A}_{4} = \begin{bmatrix} \mathbf{C}_{4} & -\mathbf{S}_{4} & \mathbf{0} & \mathbf{0} \\ \mathbf{S}_{4} & \mathbf{0} & \mathbf{C}_{4} & \mathbf{0} \\ \mathbf{0} & -\mathbf{1} & \mathbf{0} & \mathbf{1}_{5} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{1} \end{bmatrix} {}^{5}\mathbf{A}_{6} = \begin{bmatrix} \mathbf{C}_{6} & -\mathbf{S}_{6} & \mathbf{0} & \mathbf{0} \\ \mathbf{S}_{6} & \mathbf{C}_{6} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{1} & \mathbf{1}_{6} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{1} \end{bmatrix}$$

#### ABB IRB 1400: Total Transformation Matrix

![](_page_50_Figure_2.jpeg)

#### ABB IRB 1400: Forward Kinematics Solution

Given:

 $\begin{array}{c} \theta_2 \\ \theta_3 \\ \theta_4 \\ \theta_5 \end{array}$ 

θ

 $\theta_6$ 

 Point
 Required:

 Forward Kinematics

 $p_{x}=f_{x} (\theta_{1}, \theta_{2}, \theta_{3}, \theta_{4}, \theta_{5}, \theta_{6})$   $p_{y}=f_{y} (\theta_{1}, \theta_{2}, \theta_{3}, \theta_{4}, \theta_{5}, \theta_{6})$   $p_{z}=f_{z} (\theta_{1}, \theta_{2}, \theta_{3}, \theta_{4}, \theta_{5}, \theta_{6})$   $n=f_{n} (\theta_{1}, \theta_{2}, \theta_{3}, \theta_{4}, \theta_{5}, \theta_{6})$   $o=f_{o} (\theta_{1}, \theta_{2}, \theta_{3}, \theta_{4}, \theta_{5}, \theta_{6})$   $a=f_{a} (\theta_{1}, \theta_{2}, \theta_{3}, \theta_{4}, \theta_{5}, \theta_{6})$ 

$${}^{0}A_{6} = \begin{bmatrix} n_{x} & o_{x} & a_{x} & p_{x} \\ n_{y} & o_{x} & a_{x} & p_{y} \\ n_{z} & o_{x} & a_{x} & p_{z} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

## Outline

- Forward Kinematics
- Denavit-Hartenberg Algorithm
- <u>Summary</u>

## Summary

- The Denavit-Hartenberg Representation has become the standard way of representing robots and modelling their motions. The method begins with a systematic approach to assigning and labelling an orthonormal (x,y,z) coordinate system to each robot joint. It is then possible to relate one joint to the next and ultimately to assemble a complete representation of a robot's geometry.
- In assigning the x- and z-axes, you may choose either direction along the chosen line of action. Ultimately, the result of the total transformation will be the same. However, your individual matrices and parameters are similarly affected.
- It is acceptable to use additional frames to make things easier to follow. However, you may not have any fewer or more unknown variables than you have joints.

## Summary

- We can assign coordinate frames to all joints, with the following exceptions:
  - If two z-axes are parallel, there are an infinite number of common normals between them. We will pick the common normal that is colinear with the common normal of the previous joint. This will simplify the model.
  - If the z-axes of two successive joints are intersecting, there is no common normal between them (or it has a zero length). We will assign the x-axis along a line perpendicular to the plane formed by the two axes. This means that the common normal is a line perpendicular to the plane containing the two z-axes, which is the equivalent of picking the direction of the cross-product of the two z-axes. This also simplifies the model.

### Summary

- The fundamental problem of D-H representation is that since all motions are about the x- and z-axes, the method cannot represent any motion about the y-axis.
- Therefore, if there is any motion about the y-axis, the method will fail. This occurs in a number of circumstances. For example, suppose two joint axes that are supposed to be parallel are assembled with a slight deviation. The small angle between the two axes will require a motion about the y-axis. Since all real industrial robots have some degree of inaccuracy in their manufacture, their inaccuracy cannot be modeled with the D-H representation.